

Cnrs

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Berkeley, May 2016



Stain and damage localisation

Mesh dependent solution 2

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## Fracture of quasi-brittle materials

# Fracture test



### Fracture approach:

- Linear elastic fracture mechanics, cohesive crack models
- XFEM implementation, phase fields and variational approach of fracture

#### **Continuum-based approach:**

- Continuum damage, enhanced continua (non local, gradient)
- Standard FE models, TLS approach

#### Lattice approach:

 Physical aspects of fracture (continuum = thermodynamic limit), scaled lattices



$$\varepsilon_{ij} = \frac{1+\nu}{E(1-D)}\sigma_{ij} - \frac{\nu}{E(1-D)}\left[\sigma_{kk}\delta_{ij}\right]$$



















Limitations can be still observed in continuum-based approaches

- incorrect crack initiation, ahead of the crack tip;
- propagating damage fronts after failure due to non-local averaging;
- incorrect shielding effect with non-zero non-local interactions across a crack surface;
- deficiencies at capturing spalling properly in dynamics, with spalls of zero thickness when the expected spall size is below the internal length of the model



Non-locality in classical non-local models (such as integral-type):

→ The internal length is the parameter that encompasses the non-locality

$$ar{arepsilon} = rac{1}{\Omega_r(x)} \int_{\Omega} \psi_0(x,\xi) arepsilon(\xi) \mathrm{d}\xi$$
 $\psi_0(x,\xi) = \exp\left(-\left(rac{2||x-\xi||}{l_c}
ight)^2
ight)$ 
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This parameter should not be constant:





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Non-local models with varying internal length:

- D: damage  $(0 \le D \le 1)$
- Ic = f(D,d) d: boundary distance
- Stress-based non local damage model





#### → Sometimes rather empirical





Let us define an interaction as the effect on a given point x of the strain perturbation  $\epsilon^*$  located on a point  $\xi.$ 

The strain induced may be estimated energetically by:

$$A(x,\xi,arepsilon^*,a) = \sqrt{\sum_{i=1}^3 |arepsilon_i(x)|^2}$$
 (Euclidean norm)

The interaction at x due to  $\xi$  may be given by:

$$A^*(x,\xi,a) = \frac{A(x,\xi,\varepsilon^*,a)}{||\varepsilon^*||}$$

#### Assuming that this interaction governs the non-locality averaging, we get:

$$\overline{\varepsilon}_{\rm eq}(x) = \frac{1}{\Omega_r} \int_{\Omega} \psi(x,\xi) \varepsilon_{\rm eq}(\xi) d\xi \quad \text{with} \quad \psi(x,\xi) \equiv A^*(x,\xi,a) \quad \text{and} \quad \Omega_r = \int_{\Omega} A^*_0(x,\xi,a) d\xi$$

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## interaction-based non-local model

**Isotropic damage:**  $\sigma = (1 - D)\mathbb{C} : \varepsilon$ Equivalent strain:  $\varepsilon_{eq} = \sqrt{\sum_{i \in [\![1,3]\!]} \langle \varepsilon_k \rangle_+^2}$  Mazars, 1986 Nonlocal averaging:  $\overline{\varepsilon}_{eq}(x) = \frac{1}{\Omega_r} \int_{\Omega} \psi(x,\xi) \varepsilon_{eq}(\xi) d\xi$  $\psi(x,\xi) \equiv A^*(x,\xi,a) \quad \Omega_r = \int_{\Omega} A_0^*(x,\xi,a) d\xi$ **Damage evolution:**  $D(h,x) = \left[1 - (1 - A_t)\frac{\varepsilon_{D_0}}{h(x)} - A_t e^{(-B_t(h(x) - \varepsilon_{D_0}))}\right]$ 🌉 Mazars, 1986 Kuhn-Tucker condition: $\Gamma(\varepsilon,h) = \overline{\varepsilon}_{eq}(\varepsilon) - h, \quad \Gamma(\varepsilon,h) \leq 0,$  $\dot{h} \geq 0, \quad \dot{h}\Gamma(\varepsilon,h) = 0$  $h = \max(\varepsilon_{D_0}, \max(\overline{\varepsilon}_{eg}))$ 

Efficient shielding effect and assembly of small aggregates on the boundary:  $a(x) = \min(a_0\sqrt{1-D(x)}, d(x))$ 

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Damage:











# **DYERSITÉ** Dynamic failure of a bar

At complete failure, the crack opening should be independent of the element size. Assuming that the crack opening is smeared over the cracked finite element, we get:  $[U](x) \approx \varepsilon h = {\rm constant}$ 





# Meso-scale lattice model



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# **Damage Process**

#### Experiments

 Microcracks localization by acoustic emission



Grégoire et al., Int. J. Num. and Anal. Meths. Geomechanics, 2015

#### **Numerical Model**

 Identification of elements whose damage increase during the time step





# Ripley's functions

Points concentrated in 9 discs 1cm radius, spaced 2cm



### Half notched beam 700mm x 200mm

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COMPARISON SIMULATION vs EXPERIMENTAL DATA





- Need to introduce at least a length in order to bridge the gap between Continuum and fracture models
- Nonlocality is a complex issue !
- Interaction-based model provide some background
- The lattice meso-scale approach provides a consistent description of fracture
- Ripley's functions provide the evolution of a characteristic length upon localization of damage during the fracture process



Lattice approach may be implemented in more complex configurations



# Hydraulic fracturing





## Hydraulic fracturing

#### Joint at 0°





# Aknowledgements



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# Thank you for your attention

Thank you so much Zdenek...